

THE FLUID MECHANICS OF AIRWAY CLOSURE IN THE BRONCHIOLES

Francesco Romanò

Department of Fluid Mechanics and Energetics, Arts et Métiers, Lille

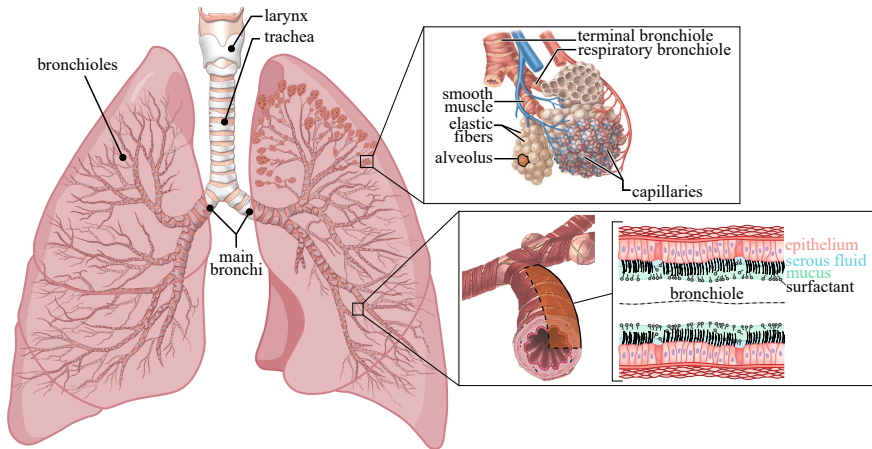
Thanks to: J.B. Grotberg, M. Muradoglu, H. Fujioka, O. Erken



Dept. of Physics, University of Rome Tor Vergata, Rome, Italy
January 16, 2023

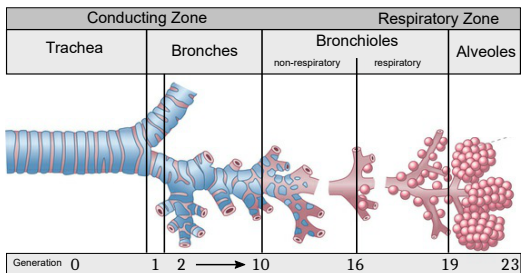
AIRWAY CLOSURE IN PHYSIOLOGY

MORPHOLOGY



AIRWAY CLOSURE IN PHYSIOLOGY

MORPHOLOGY: $d_n = d_0 \times 2^{n/3}$



Generation	Diameter (cm)	Length (cm)
0 (Trachea)	1.8	12
1	1.220	4.760
2	0.830	1.900
10	0.130	0.460
16	0.060	0.165
19	0.047	0.099
23	0.041	0.050



AIRWAY CLOSURE IN PHYSIOLOGY

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$$Bo = \frac{ga^2(\rho_L - \rho_G)}{\sigma_0}$$

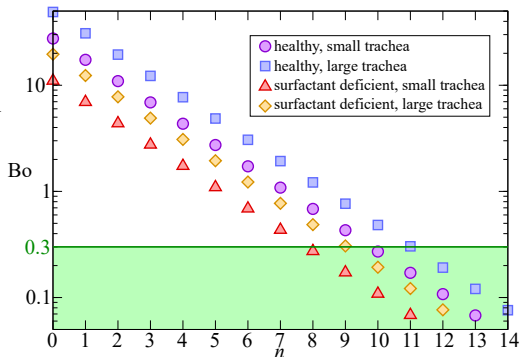
a : airway radius

ρ_L : liquid layer density

ρ_G : gas core density

g : gravity acceleration

σ_0 : liquid-gas surface tension



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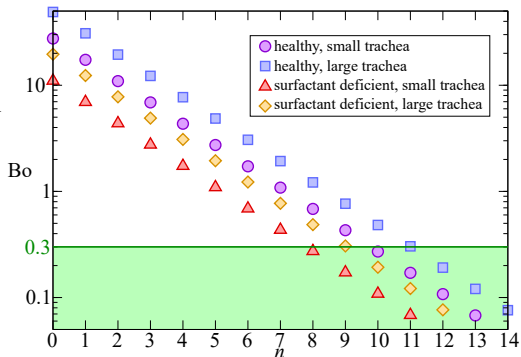
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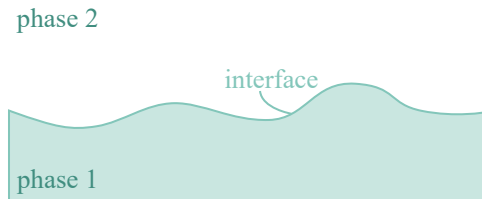


gravity negligible from ≈ 7 th generation on



SURFACE TENSION

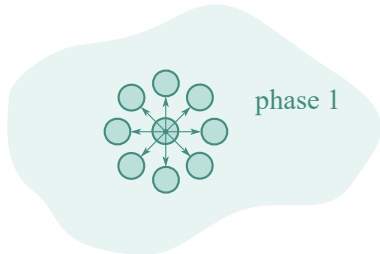
MOLECULAR SCALE



SURFACE TENSION

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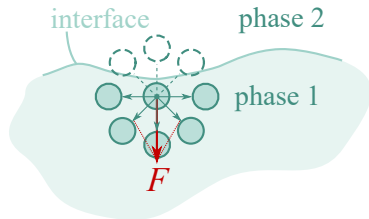
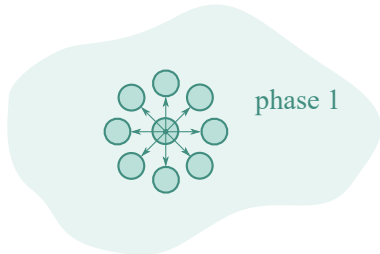
phase 2



SURFACE TENSION

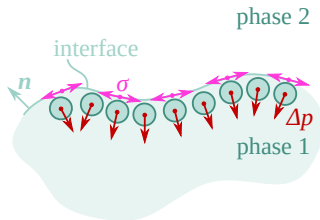
MOLECULAR SCALE

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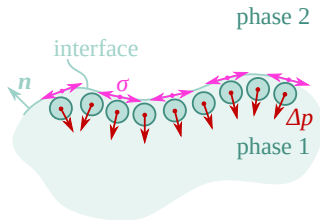
MACROSCOPIC SCALE



SURFACE TENSION

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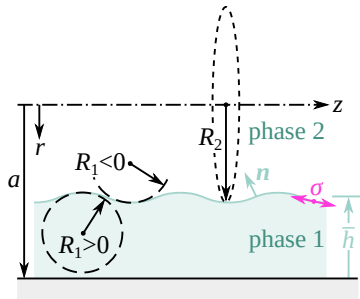
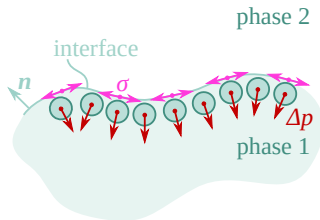
Young–Laplace equation: $\Delta p = -\sigma \nabla \cdot \mathbf{n}$



SURFACE TENSION

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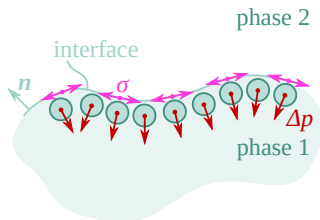
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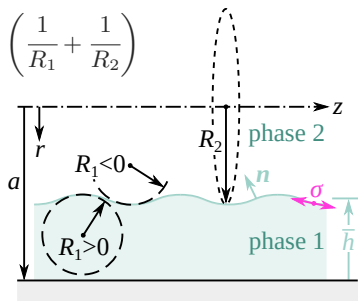
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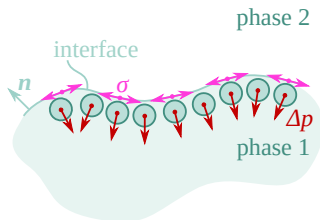
Curvature in cylindrical coordinates: $-\nabla \cdot \mathbf{n} = \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$



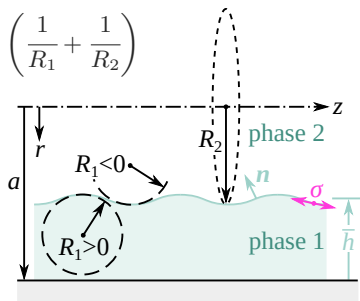
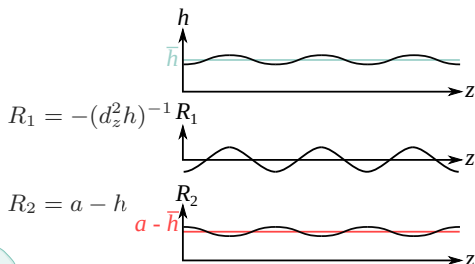
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PLATEAU–RAYLEIGH INSTABILITY

INSTABILITY MECHANISM

Assuming a varicose perturbation: $h = \bar{h}[1 + A \sin(kz)]$



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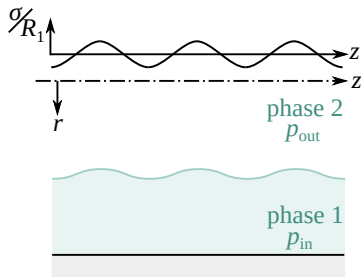


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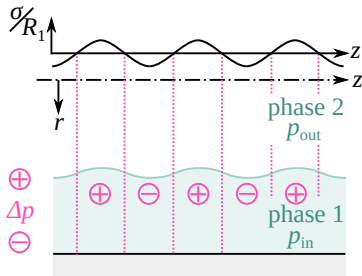


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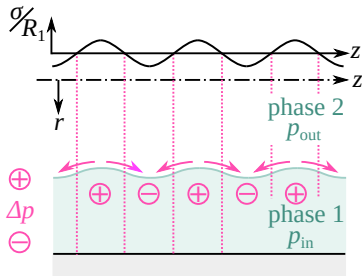


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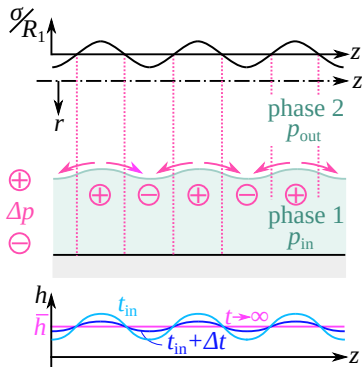


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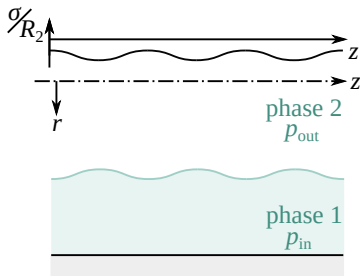
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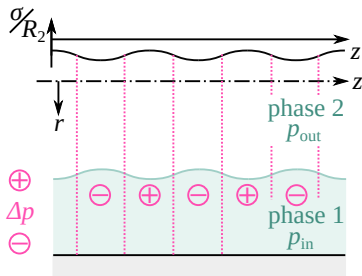
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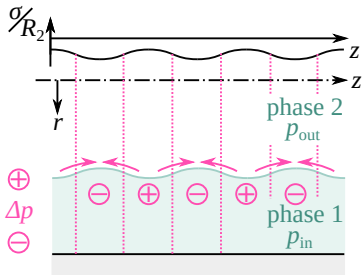
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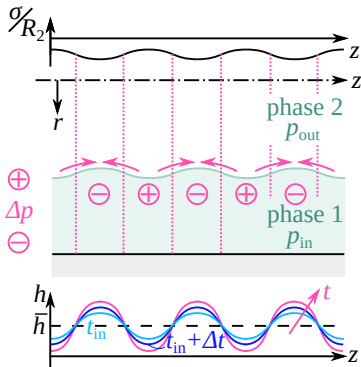
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→ The cross-sectional curvature has a destabilizing effect with $R_2 \sim a - \bar{h}$



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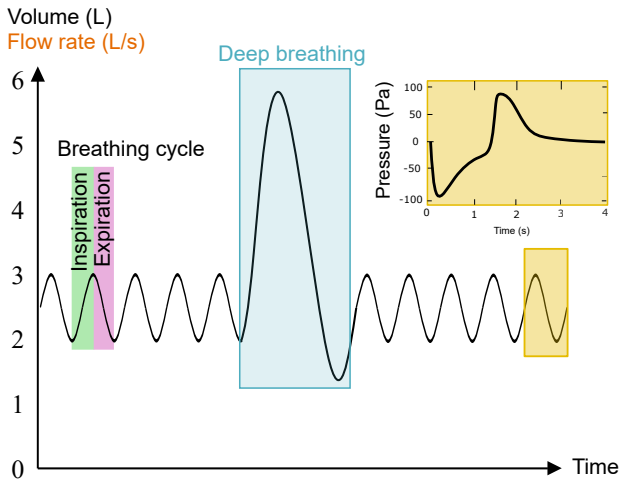
→ The cross-sectional curvature has a destabilizing effect with $R_2 \sim a - \bar{h}$

For a given \bar{h}/a one can find the critical wavenumber k_c



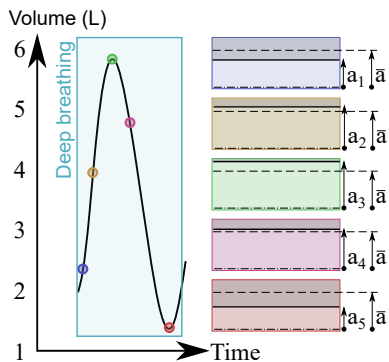
AIRWAY CLOSURE IN PHYSIOLOGY

BREATHING CYCLE



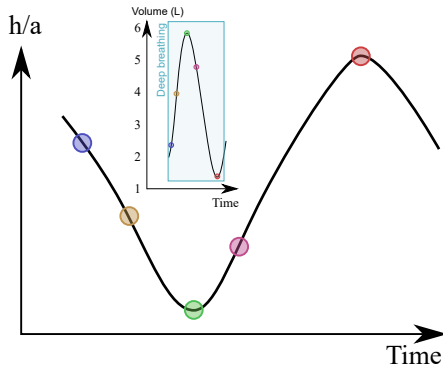
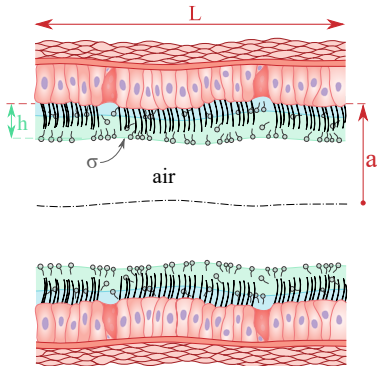
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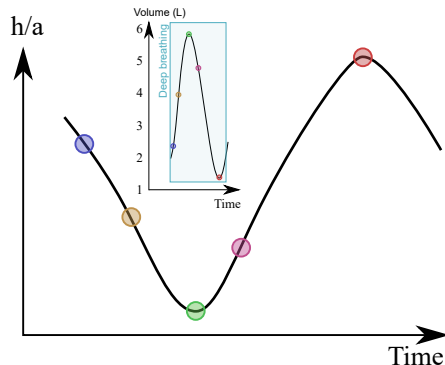
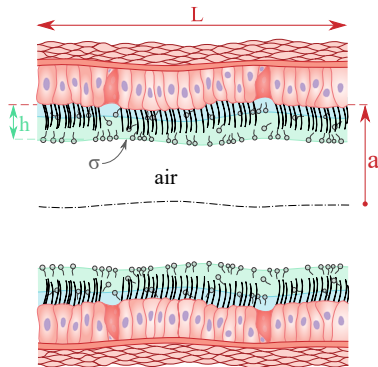
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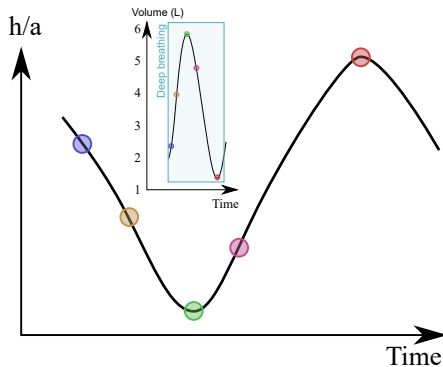
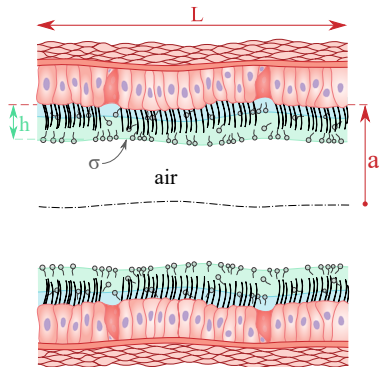
Young-Laplace equation: $\Delta p = -\sigma \nabla \cdot \mathbf{n}$

Plateau-Rayleigh instability: $2\pi(a - h)/L < 0.698$



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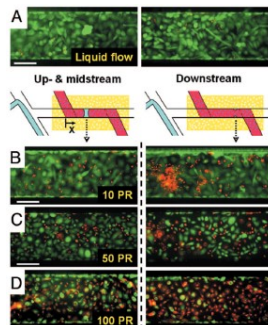
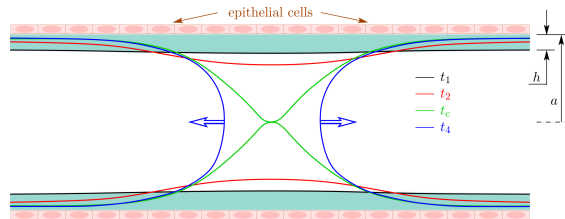
Plateau-Rayleigh instability during deep exhalation in distal airways



AIRWAY CLOSURE IN PHYSIOLOGY

IMPACT ON THE EPITHELIUM

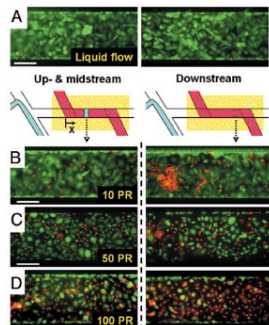
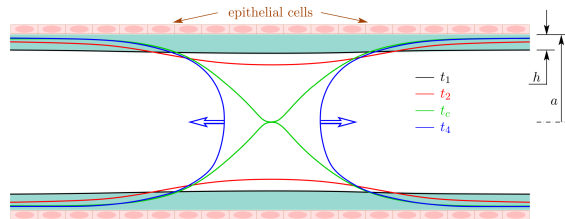
Huh et al.
PNAS (2007)



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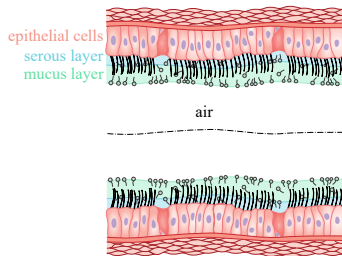


airway closure may induce lethal or sub-lethal responses for epithelial cells



MODELING CHALLENGES

PHYSIOLOGICAL AIRWAYS

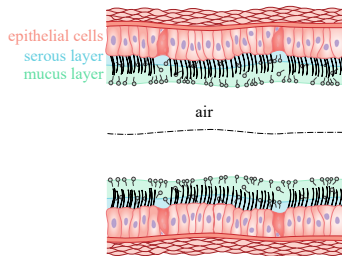


- ▷ complex multilayer structure
- ▷ ciliated surface
- ▷ fluid structure interaction
- ▷ complex multiphase flow
- ▷ non-Newtonian two-layer liquid
- ▷ surfactant dynamics



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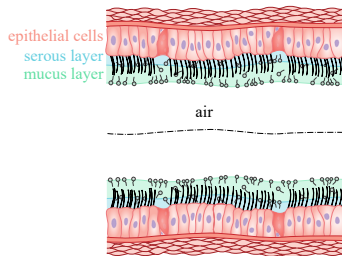
AIRWAYS MODELING

- ▷ rigid airway walls
- ▷ no through flow
- ▷ periodic conditions
- ▷ complex multiphase flow
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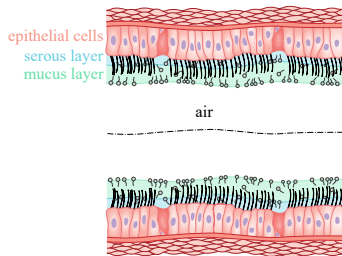
SCIENTIFIC APPROACH

- ▷ Newtonian single-layer clean



MODELING CHALLENGES

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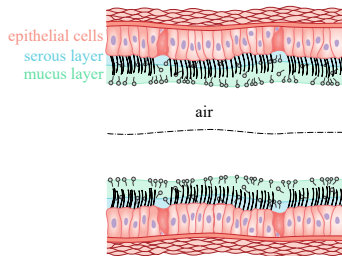
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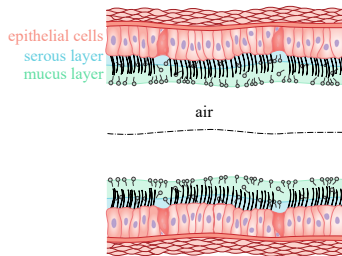
SCIENTIFIC APPROACH

- ▷ Newtonian single-layer clean
- ▷ Newtonian two-layer clean
- ▷ viscoelastic single-layer clean



MODELING CHALLENGES

PHYSIOLOGICAL AIRWAYS



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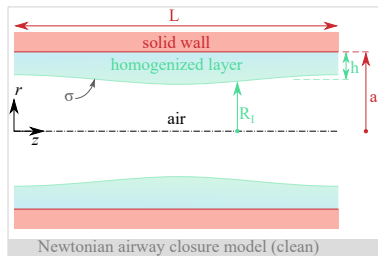
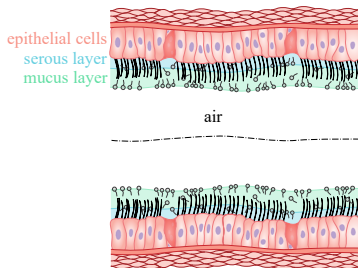
- ▷ Newtonian single-layer clean
- ▷ Newtonian two-layer clean
- ▷ viscoelastic single-layer clean
- ▷ Newtonian single-layer + surf.



NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

MATHEMATICAL MODEL



$$\nabla \cdot \mathbf{u} = 0$$

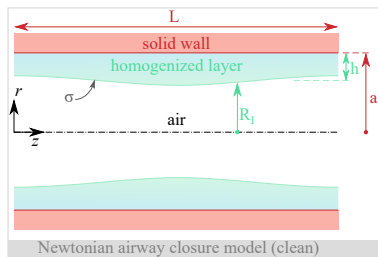
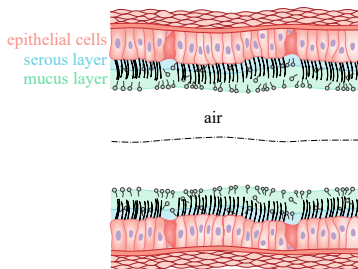
$$\text{La} \left[\frac{\partial (\tilde{\rho} \mathbf{u})}{\partial t} + \nabla \cdot (\tilde{\rho} \mathbf{u} \mathbf{u}) \right] = -\nabla p + \nabla \cdot [\tilde{\mu} (\nabla \mathbf{u} + \nabla^T \mathbf{u})] + \int_A \sigma \kappa \mathbf{n} \delta(\mathbf{x} - \mathbf{x}_f) dA$$



NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

MATHEMATICAL MODEL



$$\nabla \cdot \mathbf{u} = 0$$

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Single-field approach: $\tilde{\varrho} = \phi + \varrho(1 - \phi)$, $\tilde{\mu} = \phi + \mu(1 - \phi)$

Non-dimensional groups: $\text{La} = \frac{\sigma \rho_L a}{\mu_L^2}$, $\varrho = \frac{\rho_G}{\rho_L}$, $\mu = \frac{\mu_G}{\mu_L}$, $\lambda = \frac{L}{a}$, $\varepsilon = \frac{h}{a}$

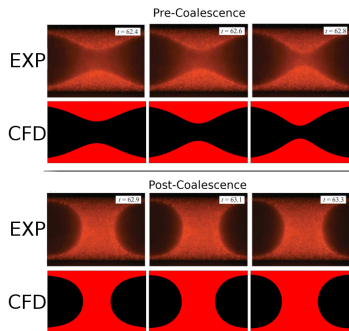
Initial perturbation: $r = R_1(t = 0) = a - h[1 - 0.1 \times \cos(2\pi z/L)]$



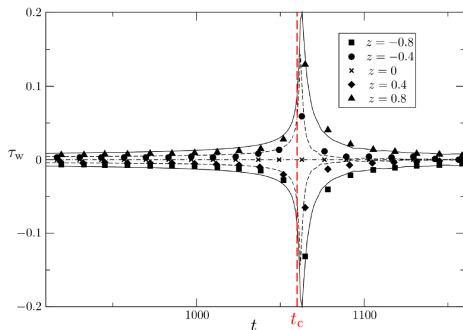
NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

COMPARISON WITH EXPERIMENTS



Exp: Bian et al., JFM (2010)
 CFD: Romanò et al., PRF (2019)



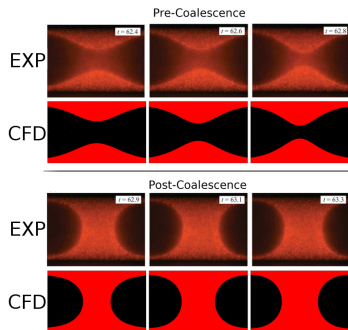
Markers: Bian et al., JFM (2010)
 Lines: Romanò et al., PRF (2019)



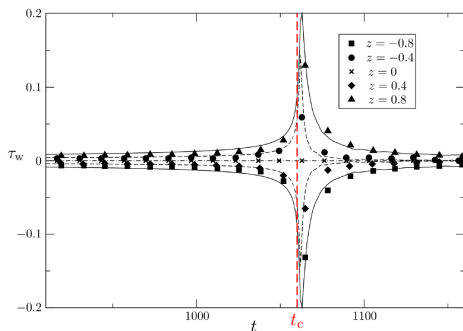
NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

COMPARISON WITH EXPERIMENTS



Exp: Bian et al., JFM (2010)
 CFD: Romanò et al., PRF (2019)



Markers: Bian et al., JFM (2010)
 Lines: Romanò et al., PRF (2019)

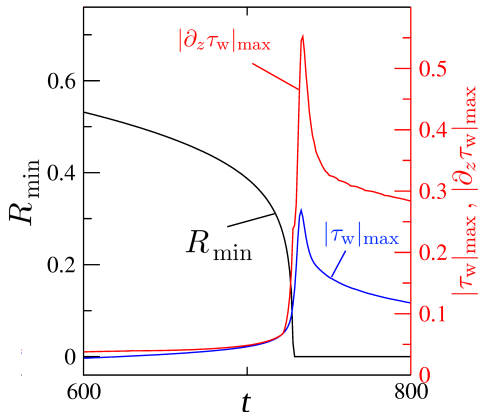
peak of shear stress right after closure (t_c)



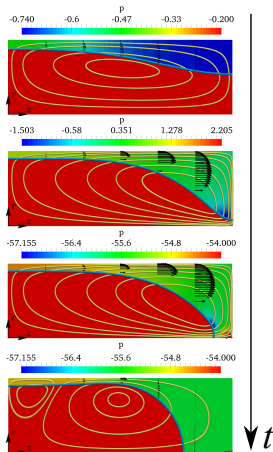
NEWTONIAN AIRWAY CLOSURE

BI-FRONTAL PLUG GROWTH

$$La = 100, \varepsilon = 0.25, \mu = 0.0015, \varrho = 0.001$$



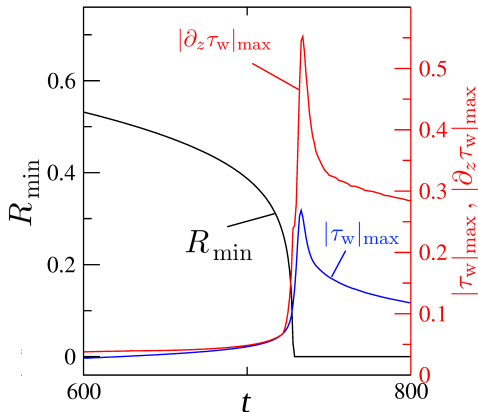
Romanò et al., PRF (2019)



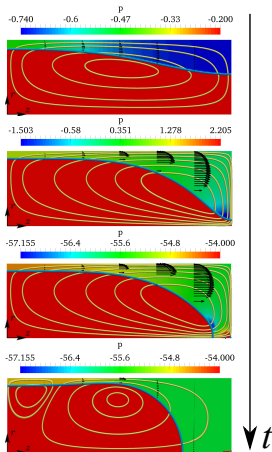
NEWTONIAN AIRWAY CLOSURE

BI-FRONTAL PLUG GROWTH

$$La = 100, \varepsilon = 0.25, \mu = 0.0015, \varrho = 0.001$$



Romanò et al., PRF (2019)



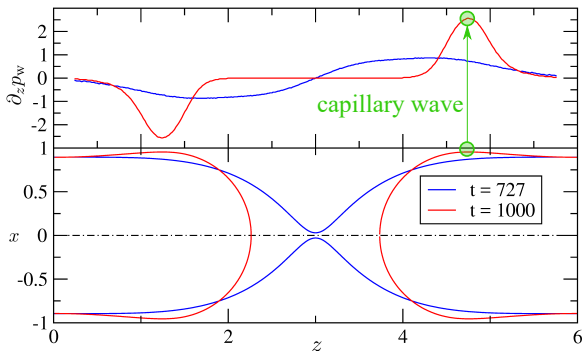
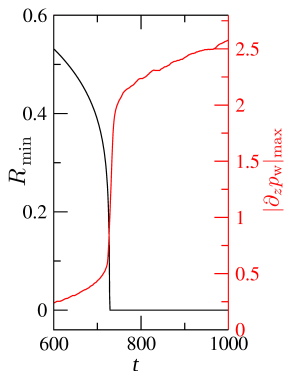
Plateau-Rayleigh instability and rapid bi-frontal plug growth



NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

BI-FRONTAL PLUG GROWTH

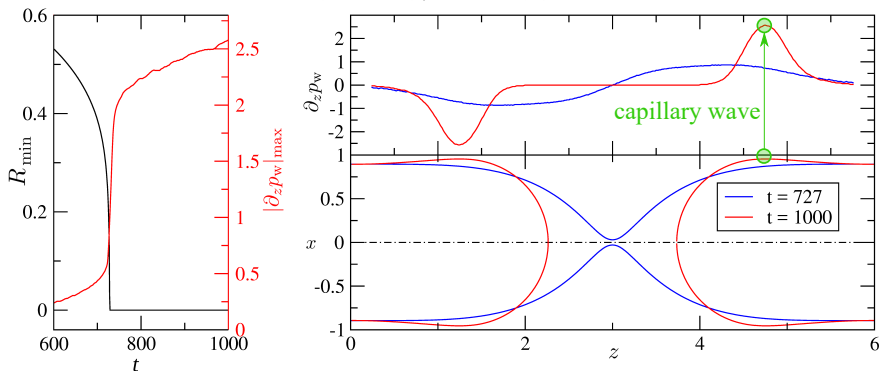
 $La = 100, \varepsilon = 0.25, \mu = 0.0015, \rho = 0.001$ 

NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

BI-FRONTAL PLUG GROWTH

$$La = 100, \varepsilon = 0.25, \mu = 0.0015, \rho = 0.001$$



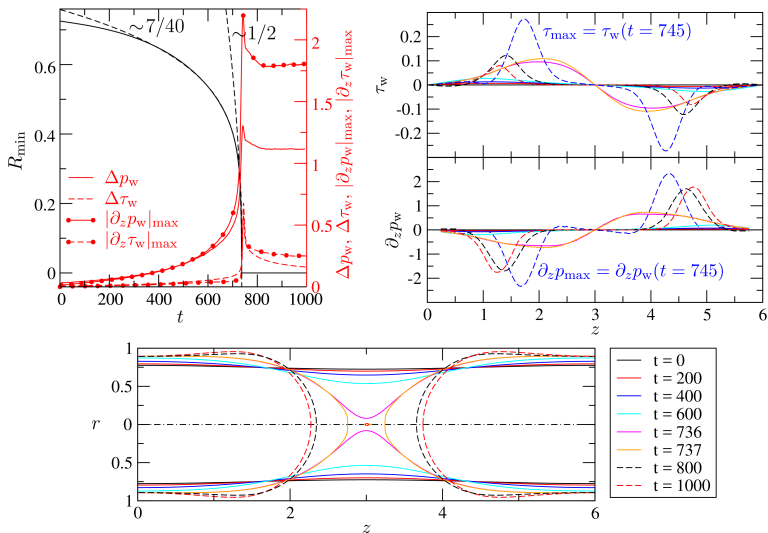
bi-frontal plug growth correlated to the wall pressure gradient



NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

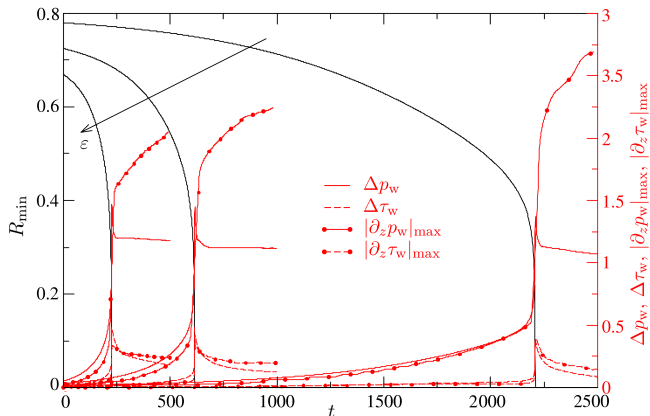
BI-FRONTAL PLUG GROWTH



NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

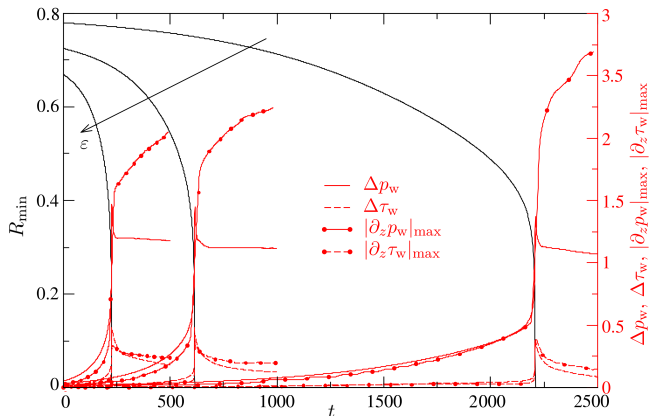
EFFECT OF FILM THICKNESS



NEWTONIAN AIRWAY CLOSURE

Romanò et al., PRF (2019)

EFFECT OF FILM THICKNESS



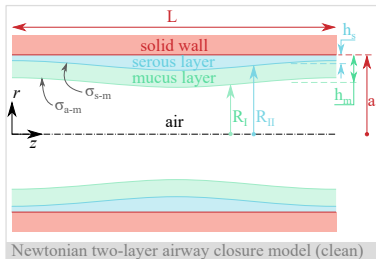
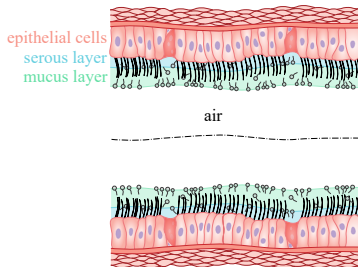
increasing ϵ speeds up the closure and reduces the wall pressure gradient



NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

MATHEMATICAL MODEL



$$\nabla \cdot \mathbf{u} = 0$$

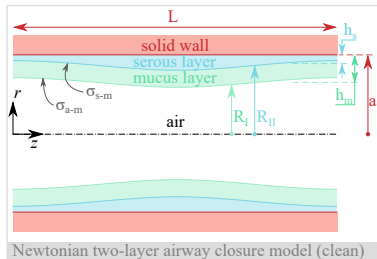
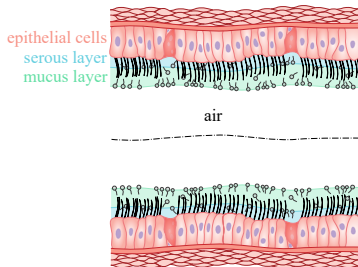
$$\text{La} \left[\frac{\partial (\tilde{\rho} \mathbf{u})}{\partial t} + \nabla \cdot (\tilde{\rho} \mathbf{u} \mathbf{u}) \right] = -\nabla p + \nabla \cdot [\tilde{\mu} (\nabla \mathbf{u} + \nabla^T \mathbf{u})] + \int_A \sigma_* \kappa \mathbf{n} \delta(\mathbf{x} - \mathbf{x}_f) dA$$



NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

MATHEMATICAL MODEL



$$\nabla \cdot \mathbf{u} = 0$$

$$\text{La} \left[\frac{\partial (\tilde{\rho} \mathbf{u})}{\partial t} + \nabla \cdot (\tilde{\rho} \mathbf{u} \mathbf{u}) \right] = -\nabla p + \nabla \cdot [\tilde{\mu} (\nabla \mathbf{u} + \nabla^T \mathbf{u})] + \int_A \sigma_* \kappa n \delta(\mathbf{x} - \mathbf{x}_f) dA$$

Single-field approach: $\tilde{\rho}(\phi_1, \phi_2)$, $\tilde{\mu}(\phi_1, \phi_2)$

Non-dimensional groups: $\text{La} = \frac{\sigma_{a-m} \rho_m a}{\mu_m^2}$, $\varrho^* = \frac{\rho_a}{\rho_m}$, $\mu^* = \frac{\mu_a}{\mu_m}$, $\lambda = \frac{L}{a}$, $\sigma = \frac{\sigma_{a-m}}{\sigma_{m-s}}$

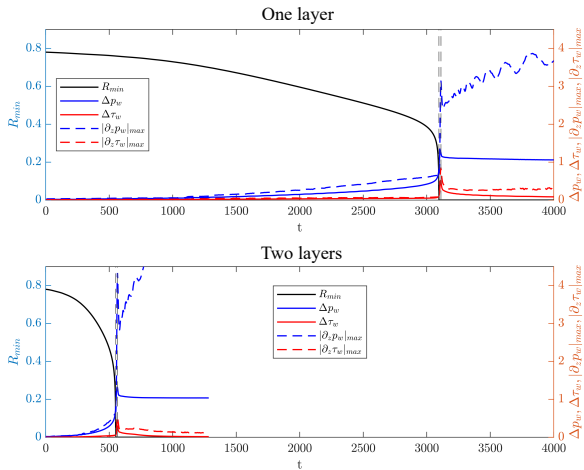
$$\varepsilon_m = \frac{h_m - h_s}{a}, \quad \varepsilon_s = \frac{h_s}{a}, \quad \varepsilon = \frac{h_m}{h_s}, \quad \mu = \frac{\mu_m}{\mu_s}, \quad \rho = \frac{\rho_m}{\rho_s}$$



NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

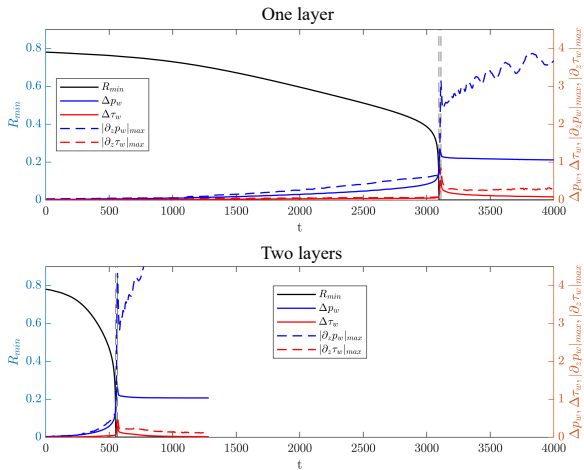
EFFECT OF SEROUS LAYER

 $La = 174, \lambda = 6, \mu = 10, \rho = 1, \sigma = 10, (\epsilon_m + \epsilon_s) = 0.2, \epsilon = 3$ 

NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

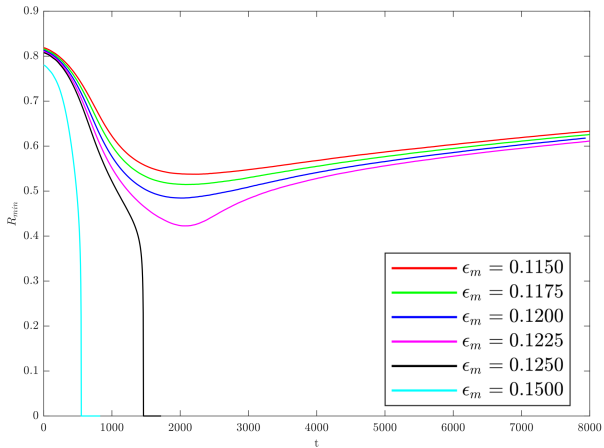
EFFECT OF SEROUS LAYER

 $La = 174, \lambda = 6, \mu = 10, \rho = 1, \sigma = 10, (\epsilon_m + \epsilon_s) = 0.2, \epsilon = 3$ including a liquid layer speeds up the airway closure ($\times 6$)

NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

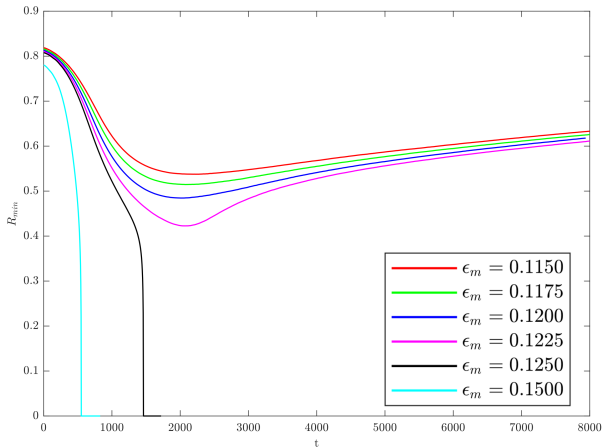
EFFECT OF MUCUS LAYER THICKNESS

 $La = 174, \lambda = 6, \mu = 10, \rho = 1, \sigma = 10, \epsilon_s = 0.05$ 

NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

EFFECT OF MUCUS LAYER THICKNESS

 $La = 174$, $\lambda = 6$, $\mu = 10$, $\rho = 1$, $\sigma = 10$, $\epsilon_s = 0.05$ 

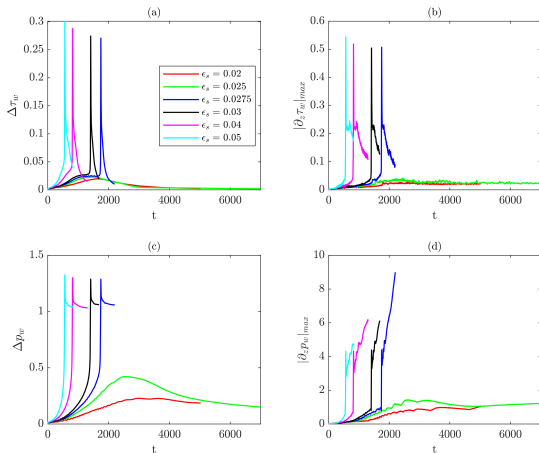
$\epsilon_m \downarrow$ stabilizes the Plateau-Rayleigh instability for $\epsilon_m = 0.1225$



NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

EFFECT OF SEROUS LAYER THICKNESS

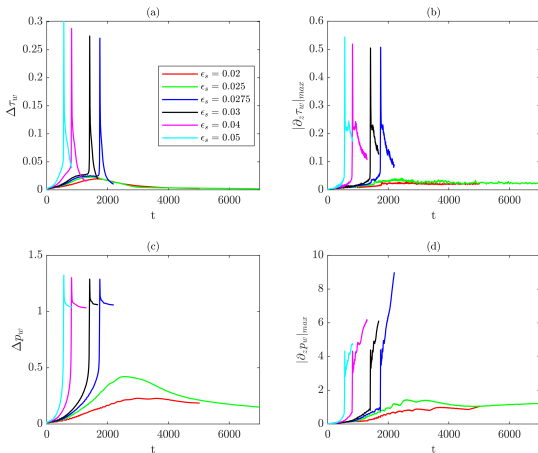
 $La = 174, \lambda = 6, \mu = 10, \rho = 1, \sigma = 10, \epsilon_m = 0.15$ 

NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

EFFECT OF SEROUS LAYER THICKNESS

$$La = 174, \lambda = 6, \mu = 10, \rho = 1, \sigma = 10, \epsilon_m = 0.15$$



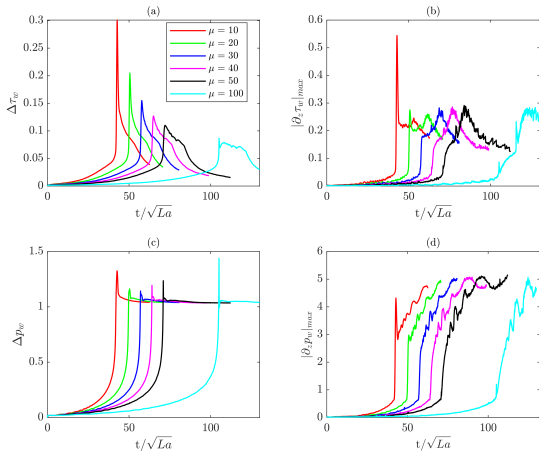
$\epsilon_s \downarrow$ stabilizes the Plateau-Rayleigh instability for $\epsilon_s = 0.025$



NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

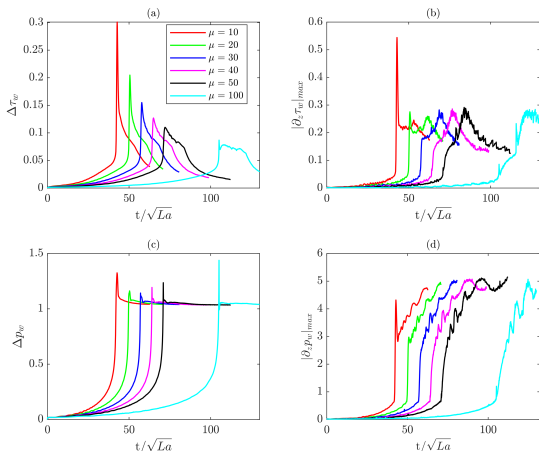
EFFECT OF VISCOSITY RATIO

 $La = 174$, $\lambda = 6$, $\rho = 1$, $\sigma = 10$, $(\epsilon_m + \epsilon_s) = 0.2$, $\epsilon = 3$ 

NEWT. TWO-LAYER AIRWAY CLOSURE

Erken et al., JFM (2022)

EFFECT OF VISCOSITY RATIO

 $La = 174$, $\lambda = 6$, $\rho = 1$, $\sigma = 10$, $(\epsilon_m + \epsilon_s) = 0.2$, $\epsilon = 3$ 

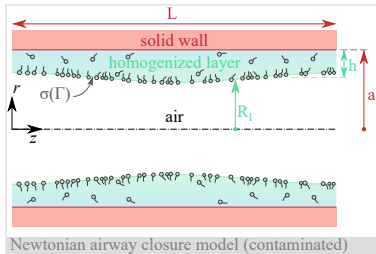
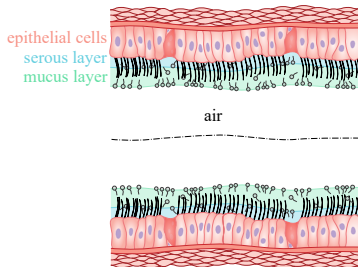
$\mu \uparrow$ reduces the shear stresses and does not impact the normal stresses



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., submit.

MATHEMATICAL MODEL



$$\nabla \cdot \mathbf{u} = 0$$

$$\text{La} \left[\frac{\partial (\tilde{\varrho} \mathbf{u})}{\partial t} + \nabla \cdot (\tilde{\varrho} \mathbf{u} \mathbf{u}) \right] = -\nabla p + \nabla \cdot [\tilde{\mu} (\nabla \mathbf{u} + \nabla^T \mathbf{u})] + \int_A \sigma(\Gamma) \kappa n \delta(\mathbf{x} - \mathbf{x}_f) dA + \int_A \nabla_s \sigma(\Gamma) \delta(\mathbf{x} - \mathbf{x}_f) dA$$

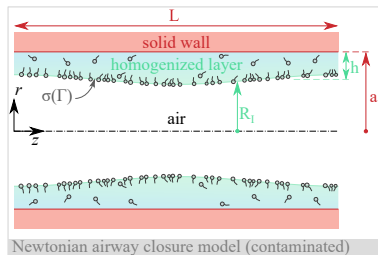
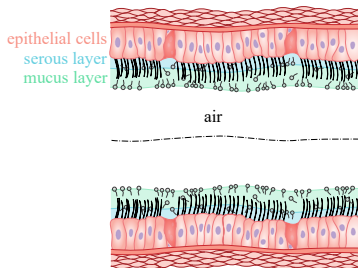
Single-field approach: $\tilde{\varrho} = \phi + \varrho(1 - \phi)$, $\tilde{\mu} = \phi + \mu(1 - \phi)$



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., submit.

MATHEMATICAL MODEL



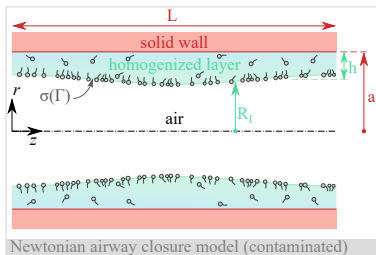
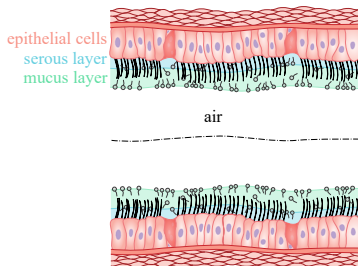
$$\sigma = \begin{cases} (1 - \beta\Gamma) & \text{if } \Gamma < 1, \\ (1 - \beta) \exp \left[\frac{\beta(1 - \Gamma)}{1 - \beta} \right] & \text{if } \Gamma \geq 1. \end{cases} \quad \text{where } \beta = \frac{\mathcal{R}T\Gamma_\infty}{\sigma_0}$$



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., submit.

MATHEMATICAL MODEL



$$\frac{1}{A} \frac{D(\Gamma A)}{Dt} = \frac{1}{Sc_s La} \nabla_s^2 \Gamma + \dot{S}_\Gamma,$$

$$\frac{\partial C}{\partial t} + \nabla \cdot (C \mathbf{u}) = \frac{1}{Sc_s La} \nabla \cdot (\tilde{D} \nabla C) + \dot{S}_C,$$

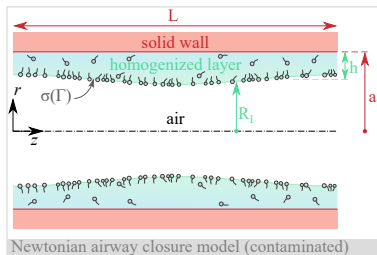
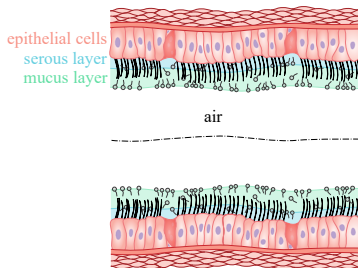
$$\dot{S}_\Gamma = \begin{cases} \frac{K_a}{La Sc_s} C_s (1 - \Gamma) - \frac{K_d}{La Sc_s} \Gamma & \text{if } \Gamma < 1, \\ -\frac{K_d}{La Sc_s} \Gamma & \text{if } \Gamma \geq 1, \end{cases}$$



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., submit.

MATHEMATICAL MODEL



Non-dimensional groups: $La = \frac{\sigma_0 \rho_L a}{\mu_L^2}$, $\varrho = \frac{\rho_G}{\rho_L}$, $\mu = \frac{\mu_G}{\mu_L}$, $\lambda = \frac{L}{a}$, $\varepsilon = \frac{h}{a}$,

$$\beta = \frac{\mathcal{R}T\Gamma_\infty}{\sigma_0}, \quad Sc = \frac{\mu_L}{\rho_L D_L}, \quad Sc_s = \frac{\mu_L}{\rho_L D_S},$$

$$K_a = \frac{k_a C_{cmc} a^2}{D_S}, \quad K_d = \frac{k_a a^2}{D_S}, \quad \chi = \frac{\Gamma_\infty}{C_{cmc} a},$$

Initial perturbation: $r = R_I(t=0) = a - h[1 - 0.1 \times \cos(2\pi z/L)]$

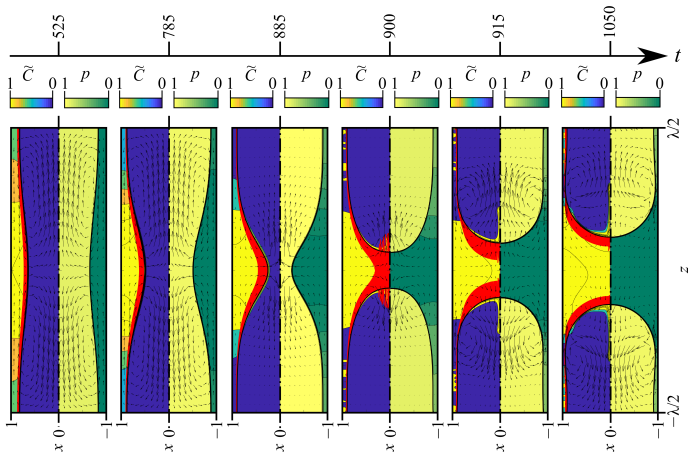


NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

DYNAMICS OF THE SURFACTANT

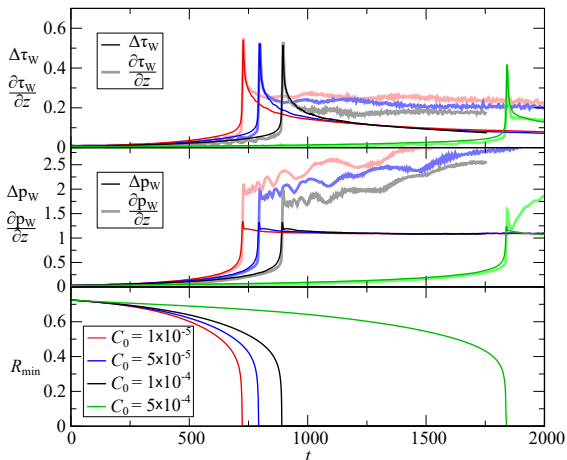
$La = 100$, $\beta = 0.7$, $Sc = 10$, $Sc_s = 100$, $K_a = 10^4$, $K_d = 10^2$, $\chi = 0.01$,
 $C_0 = 10^{-4}$, $\varepsilon = 0.25$



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

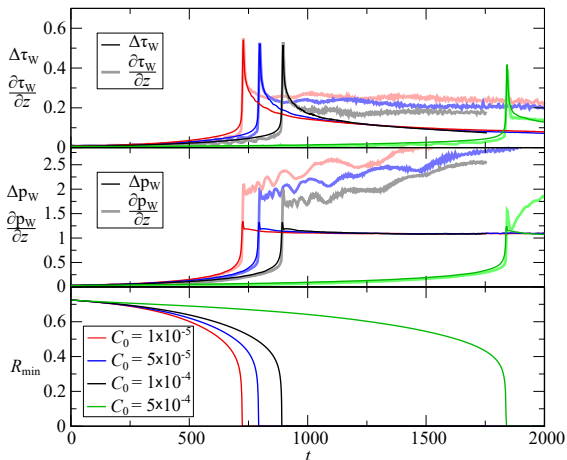
EFFECT OF SURFACTANT CONCENTRATION

 $La = 100$, $\beta = 0.7$, $Sc = 10$, $Sc_s = 100$, $K_a = 10^4$, $K_d = 10^2$, $\chi = 0.01$, $\varepsilon = 0.25$


NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

EFFECT OF SURFACTANT CONCENTRATION

 $La = 100, \beta = 0.7, Sc = 10, Sc_s = 100, K_a = 10^4, K_d = 10^2, \chi = 0.01, \varepsilon = 0.25$


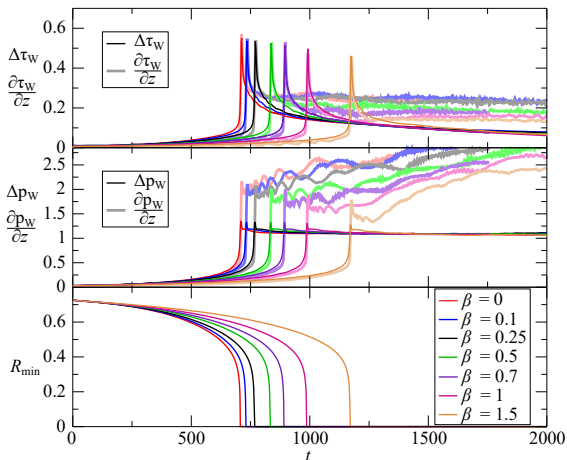
increasing C_0 slows down the closure and reduces the stresses



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

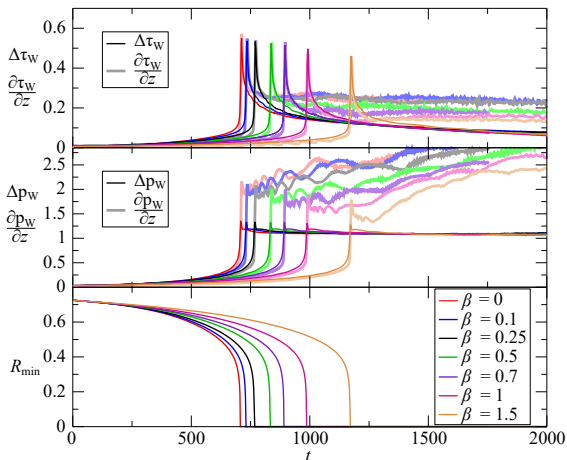
EFFECT OF SURFACTANT ELASTICITY PARAMETER

 $La = 100, \chi = 0.01, Sc = 10, Sc_s = 100, K_a = 10^4, K_d = 10^2, C_0 = 10^{-4}, \varepsilon = 0.25$


NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

EFFECT OF SURFACTANT ELASTICITY PARAMETER

 $La = 100, \chi = 0.01, Sc = 10, Sc_s = 100, K_a = 10^4, K_d = 10^2, C_0 = 10^{-4}, \varepsilon = 0.25$


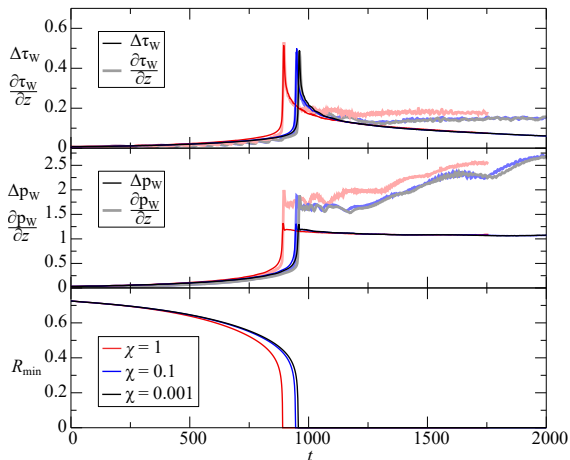
$\beta \uparrow$ slows down the closure and reduces the stresses



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

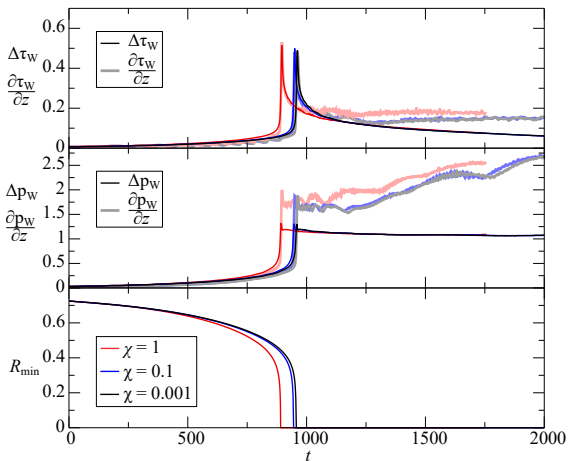
EFFECT OF PENETRATION DEPTH

 $La = 100, \beta = 0.7, Sc = 10, Sc_s = 100, K_a = 10^4, K_d = 10^2, C_0 = 10^{-4}, \varepsilon = 0.25$


NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

EFFECT OF PENETRATION DEPTH

 $La = 100, \beta = 0.7, Sc = 10, Sc_s = 100, K_a = 10^4, K_d = 10^2, C_0 = 10^{-4}, \varepsilon = 0.25$


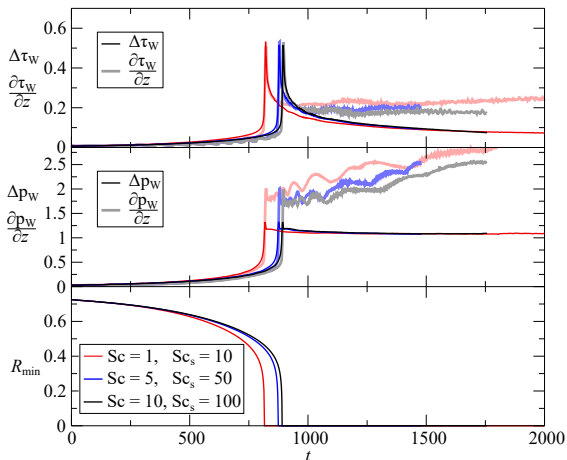
χ has little impact on the airway closure



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

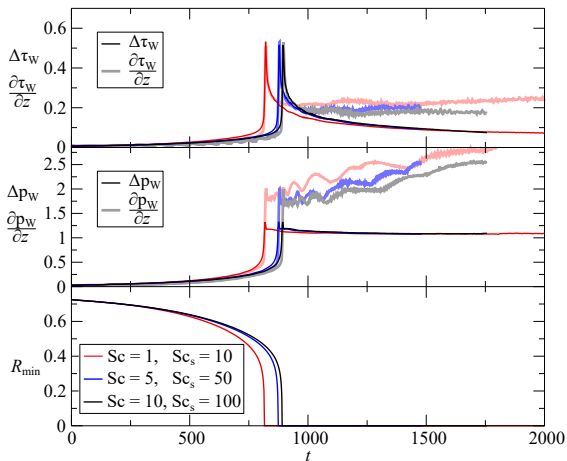
EFFECT OF SCHMIDT NUMBERS

 $La = 100$, $\chi = 0.01$, $\beta = 0.7$, $K_a = 10^4$, $K_d = 10^2$, $C_0 = 10^{-4}$, $\varepsilon = 0.25$


NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

EFFECT OF SCHMIDT NUMBERS

 $La = 100$, $\chi = 0.01$, $\beta = 0.7$, $K_a = 10^4$, $K_d = 10^2$, $C_0 = 10^{-4}$, $\varepsilon = 0.25$


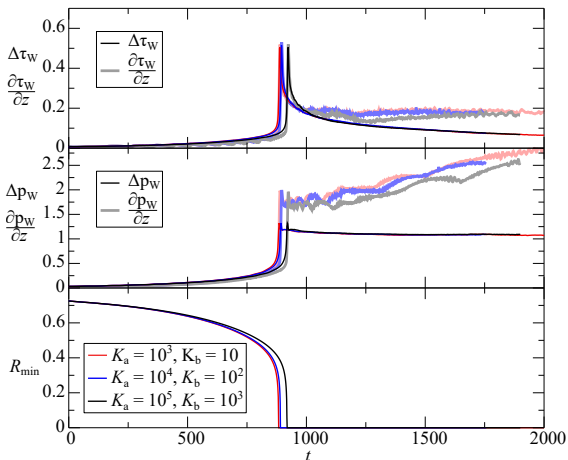
Sc and Sc_s have little impact on the airway closure



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

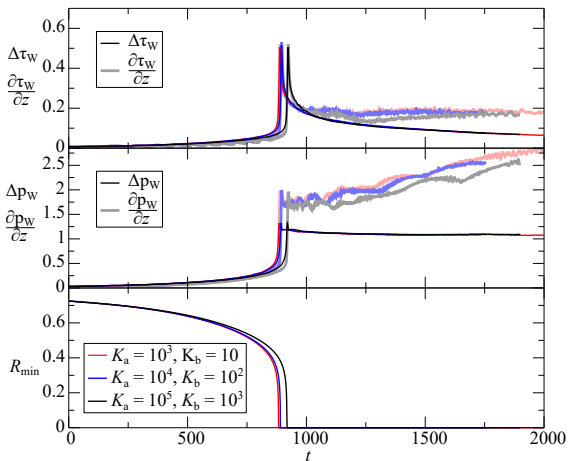
EFFECT OF ADSORPTION AND DESORPTION COEFFICIENTS

 $La = 100$, $\chi = 0.01$, $\beta = 0.7$, $Sc = 10$, $Sc_s = 100$, $C_0 = 10^{-4}$, $\varepsilon = 0.25$ 

NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

EFFECT OF ADSORPTION AND DESORPTION COEFFICIENTS

 $La = 100$, $\chi = 0.01$, $\beta = 0.7$, $Sc = 10$, $Sc_s = 100$, $C_0 = 10^{-4}$, $\varepsilon = 0.25$ 

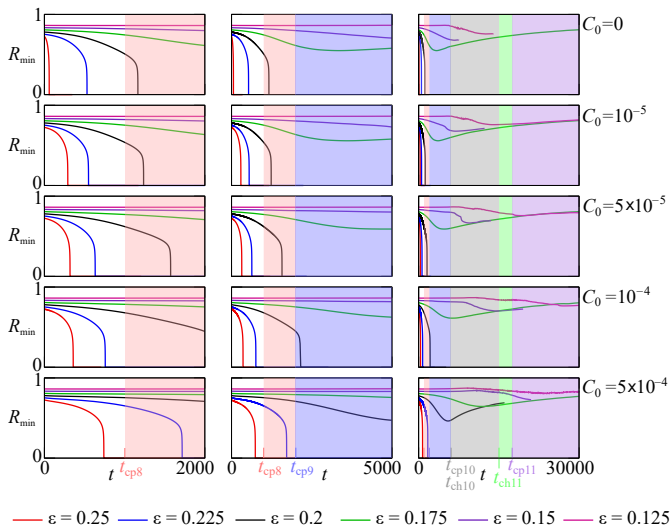
K_a and K_d have little impact on the airway closure



NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

STABILITY ANALYSIS

 $La = 100, \chi = 0.01, \beta = 0.7, Sc = 10, Sc_s = 100, K_a = 10^4, K_d = 10^2$


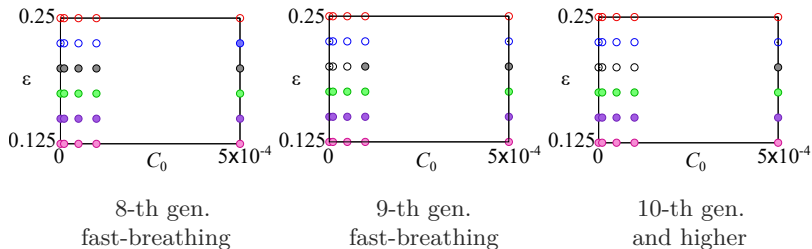
NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

STABILITY ANALYSIS

 $La = 100$, $\chi = 0.01$, $\beta = 0.7$, $Sc = 10$, $Sc_s = 100$, $K_a = 10^4$, $K_d = 10^2$

● = physiologically stable ○ = physiologically unstable



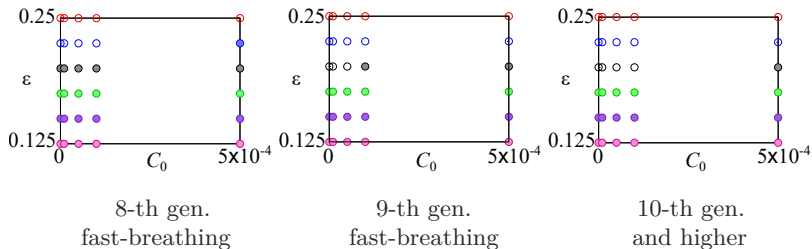
NEWT. AIRWAY CLOSURE + SURF.

Romanò et al., PRF (2022)

STABILITY ANALYSIS

 $La = 100$, $\chi = 0.01$, $\beta = 0.7$, $Sc = 10$, $Sc_s = 100$, $K_a = 10^4$, $K_d = 10^2$

● = physiologically stable ○ = physiologically unstable



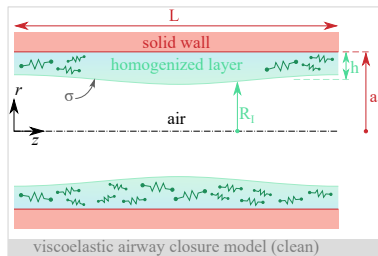
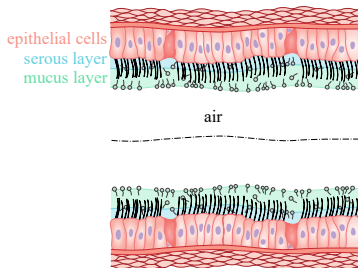
surfactant replacement can stabilize and shift closure to higher generations



VISCOELASTIC AIRWAY CLOSURE

Romanò et al., JFM (2021)

MATHEMATICAL MODEL



$$\nabla \cdot \mathbf{u} = 0$$

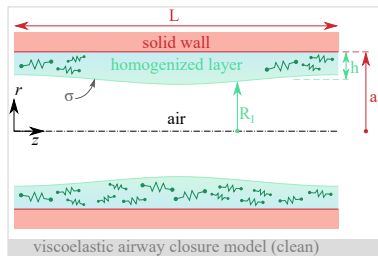
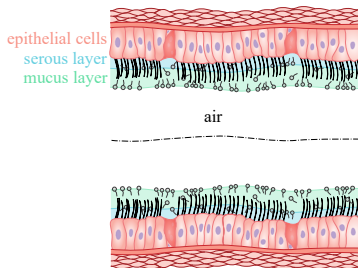
$$\text{La} \left[\frac{\partial (\tilde{\rho} \mathbf{u})}{\partial t} + \nabla \cdot (\tilde{\rho} \mathbf{u} \mathbf{u}) \right] = -\nabla p + \nabla \cdot \tilde{\boldsymbol{\tau}} + \int_A \sigma \kappa \mathbf{n} \delta(\mathbf{x} - \mathbf{x}_f) dA$$



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Single-field approach: $\tilde{\rho} = \phi + \rho(1 - \phi)$, $\tilde{\boldsymbol{\tau}} = [\mu_S \phi + \mu(1 - \phi)] (\nabla \mathbf{u} + \nabla^T \mathbf{u}) + \phi \mathbf{S}$

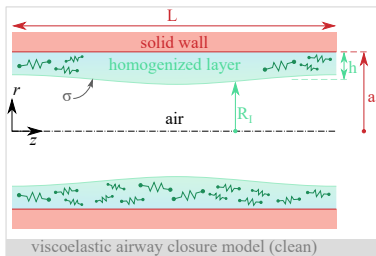
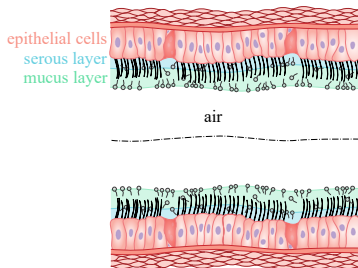
Oldroyd-B: $\text{We} [\partial_t \mathbf{S} + (\mathbf{u} \cdot \nabla) \mathbf{S} - (\nabla \mathbf{u}) \mathbf{S} - \mathbf{S} (\nabla^T \mathbf{u})] + \mathbf{S} = \mu_P (\nabla \mathbf{u} + \nabla^T \mathbf{u})$



VISCOELASTIC AIRWAY CLOSURE

Romanò et al., JFM (2021)

MATHEMATICAL MODEL



Non-dimensional groups: $La = \frac{\sigma \rho_L a}{\mu_L^2}$, $\varrho = \frac{\rho_G}{\rho_L}$, $\mu = \frac{\mu_G}{\mu_L}$, $\lambda = \frac{L}{a}$, $\varepsilon = \frac{h}{a}$

$We = \frac{\Lambda \sigma}{a \mu_L}$, $\mu_S = \frac{\mu_{L,S}}{\mu_L}$, $\mu_P = 1 - \mu_S$, (\mathcal{L}^2 for FENE-CR)

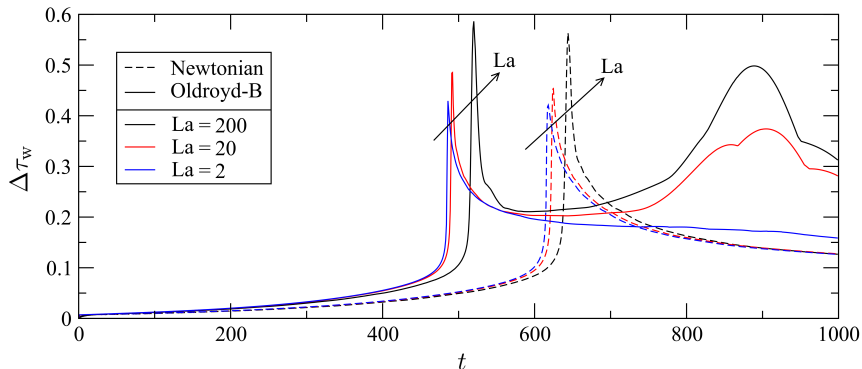
Initial perturbation: $r = R_I(t = 0) = a - h[1 - 0.1 \times \cos(2\pi z/L)]$



VISCOELASTIC AIRWAY CLOSURE

Romanò et al., JFM (2021)

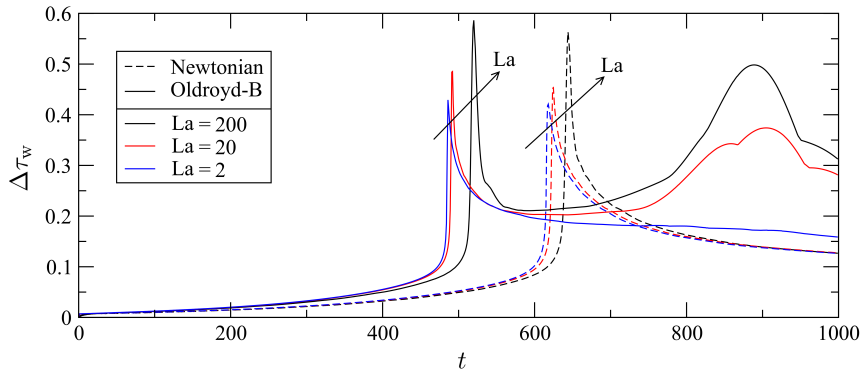
EFFECT OF VISCOELASTICITY (OLDROYD-B)

 $\mu = 1.5 \times 10^{-4}$, $\varrho = 10^{-3}$, $\epsilon = 0.25$, $\lambda = 6$, $\mu_S = 0.5$, $We = 100$ 

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qualitative difference between Newtonian and viscoelastic

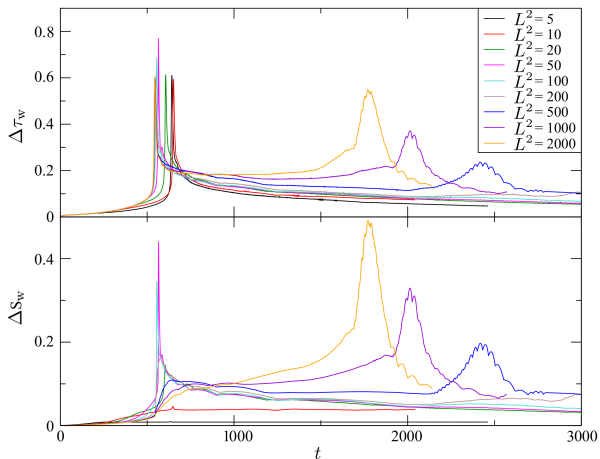


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Romanò et al., JFM (2021)

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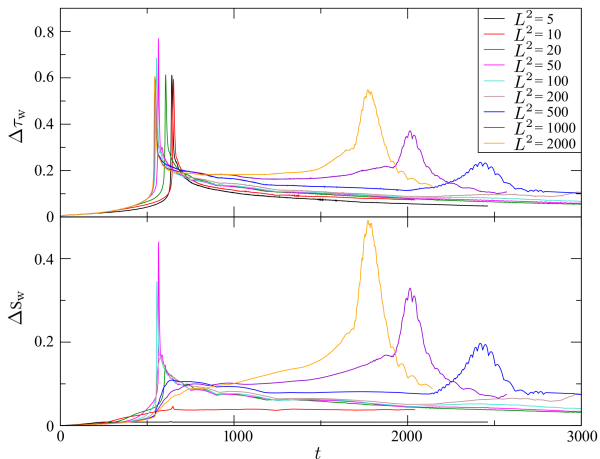


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Romanò et al., JFM (2021)

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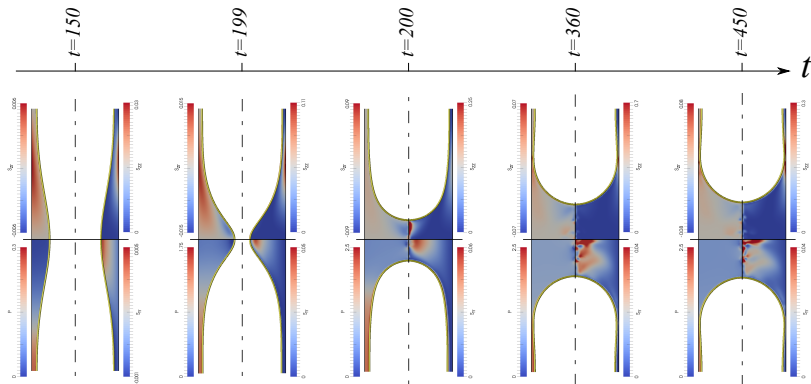
second hump robust to viscoelastic model



VISCOELASTIC AIRWAY CLOSURE

Romanò et al., JFM (2021)

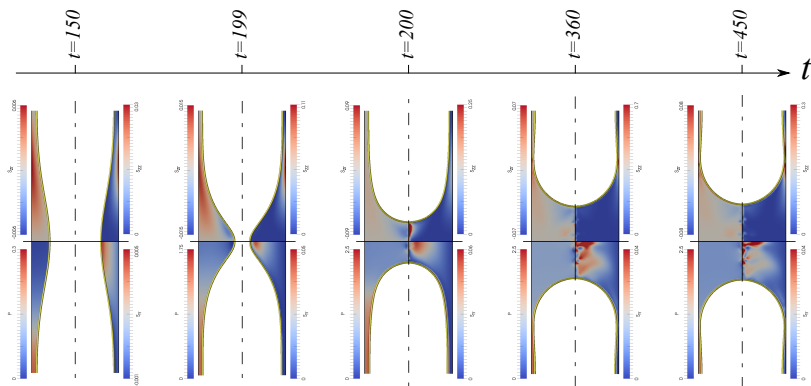
VISCOELASTIC INSTABILITY MECHANISM

 $La = 2$, $\mu = 1.5 \times 10^{-4}$, $\rho = 10^{-3}$, $\epsilon = 0.25$, $\lambda = 6$, $\mu_S = 0.25$, $We = 500$


VISCOELASTIC AIRWAY CLOSURE

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 $La = 2$, $\mu = 1.5 \times 10^{-4}$, $\rho = 10^{-3}$, $\epsilon = 0.25$, $\lambda = 6$, $\mu_S = 0.25$, $We = 500$


instability due to curvature of the streamlines

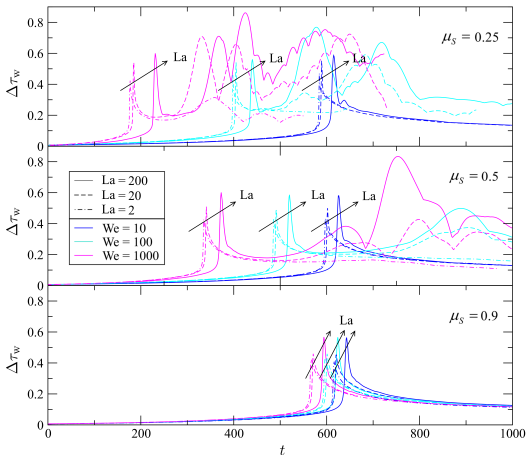


VISCOELASTIC AIRWAY CLOSURE

Romanò et al., JFM (2021)

EFFECT OF FLOW AND POLYMERIC PARAMETERS

$$\mu = 1.5 \times 10^{-4}, \varrho = 10^{-3}, \epsilon = 0.25, \lambda = 6,$$

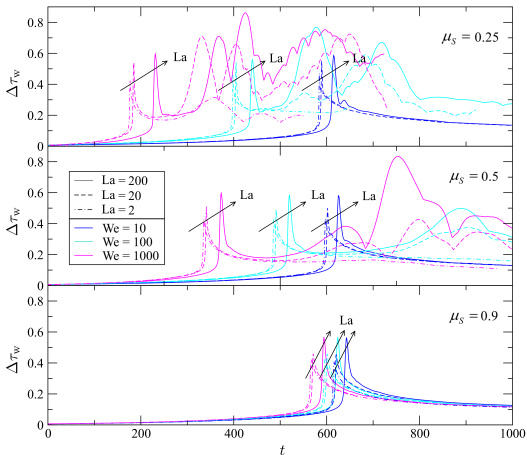


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Romanò et al., JFM (2021)

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the instability depends on La , We , and μ_s

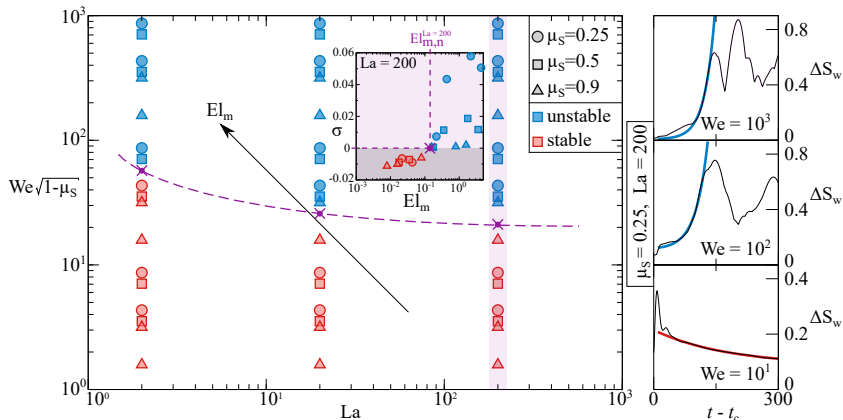


VISCOELASTIC AIRWAY CLOSURE

Romanò et al., JFM (2021)

ELASTO-INERTIAL INSTABILITY

$$\mu = 1.5 \times 10^{-4}, \varrho = 10^{-3}, \epsilon = 0.25, \lambda = 6,$$

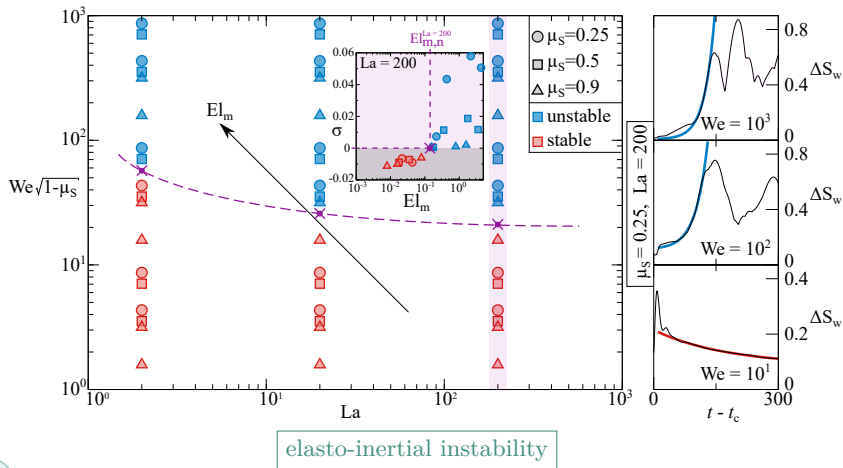


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CONCLUSIONS

Support from NIH (R01-HL136141) and from TUKITAK (119M513)



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- ▷ At high We , elasto-inertial instability induces severe extra stresses
- ▷ Surfactant reduces the wall stresses and postpones the airway closure



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